In the Claims:

This listing of claims will replace all prior versions, and listings, of claims in the application.

1. (original) A high-strength hot-rolled steel sheet excellent in shape fixability, wherein ferrite or bainite is the maximum phase in terms of percent volume,

satisfying all of the following at least at 1/2 of the sheet thickness:

(1) a mean value of X-ray random intensity ratios of a group of {100}<011> to {223}<110> orientations is 2.5 or more,

(2) a mean value of X-ray random intensity ratio of three orientations of {554}<225>, {111}<112>, {111}<110> is 3.5 or less,

(3) X-ray random intensity ratio of {100}<011> is larger than that of {211}<011>,

(4) X-ray random intensity ratio of {100}<011> is 2.5 or more,

having at least one of an r-value in a rolling direction and the r-value in a direction perpendicular to the rolling direction is 0.7 or less,

having anisotropy of uniform elongation $\Delta uE1$ is 4% or less,

having an anisotropy of local elongation $\Delta LE1$ is 2% or more, and

having an $\Delta uE1$ which is $\Delta LE1$ or less, where:

$\Delta uE1 = \{ |uE1(L) - uE1(45°)| + |uE1(C) - uE1(45°)| \}/2$

$\Delta LE1 = \{ |LE1(L) - LE1(45°)| + |LE1(C) - LE1(45°)| \}/2$

uE1(L): Uniform elongation in a rolling direction

uEl(C): Uniform elongation in a transverse direction

uEl(45°): Uniform elongation in a 45° direction

LEl(L): Local elongation in a rolling direction

LEl(C): Local elongation in a transverse direction

LEl(45°): Local elongation in a 45° direction.

2. (original)   A high-strength hot-rolled steel sheet excellent in shape fixability according to claim 1, characterized in that an occupancy rate of iron carbide, diameter of which is 0.2 μm or more, is 0.3% or less.

3. (original)   A high-strength hot-rolled steel sheet excellent in shape fixability according to claim 1, characterized in that an aging index AI is 8 MPa or more.

4. (original)   A high-strength hot-rolled steel sheet excellent in shape fixability according to claim 1, characterized by containing, in terms of weight %,

C: 0.01 to 0.2%,

Si: 0.001 to 2.5%,

Mn: 0.01 to 2.5%,

P: 0.2% or less,

S: 0.03% or less,

Al: 0.01 to 2%,

N: 0.01% or less, and

O: 0.01% or less

and remainder Fe and unavoidable impurities.

5. (original)   A high-strength hot-rolled steel sheet excellent in shape fixability according to claim 4, characterized by further containing at least one or more element selected from Nb, Ti and V with a total of 0.001 to 0.8%, in terms of weight %.

6. (currently amended)   A high-strength hot-rolled steel sheet excellent in shape fixability according to claim 4 ~~or 5~~, characterized by further containing at least one or more, in terms of weight %,

B: 0.01% or less,

Mo: 1% or less,

Cr: 1% or less,

Cu: 2% or less,

Ni: 1% or less,

Sn: 0.2% or less,

Co: 2% or less,

Ca: 0.0005 to 0.005%,

Rem: 0.001 to 0.05%,

Mg: 0.0001 to 0.05%,

Ta: 0.0001 to 0.05%.

7. (original) A high-strength hot-rolled steel sheet excellent in shape fixability according to claim 1, characterized by containing, in terms of weight %,

C: 0.02 to 0.3%,

at least one or more element selected from the following group consisting of, total 0.1 to 3.5%, in terms of weight %,

Mn: 0.05 to 3%,

NI: 3% or less,

Cr: 3% or less,

Cu: 3% or less,

Mo: 1% or less,

Co: 3% or less and

Sn: 0.2% or less,

at least one or both consisting of, total 0.02 to 3% in terms of weight %,

Si: 3% or less and

Al: 3% or less

and remainder Fe and unavoidable impurities, and having multi-phase structure, wherein ferrite or bainite is the maximum phase in terms of percent volume, and a percent volume of martensite is 1 to 25%.

8. (original) A high-strength hot-rolled steel sheet excellent in shape fixability according to claim 7, characterized by containing, in terms of weight %, at least one or more element selected from Nb, Ti and V with a total of 0.001 to 0.8%, in terms of weight %.

9. (currently amended) A high-strength hot-rolled steel sheet excellent in shape fixability according to claim 7 ~~or 8~~, characterized by further containing at the least of one or more element selected from the following group consisting of, in terms of weight %,

P: 0.2% or less,

B: 0.01% or less,

Ca: 0.0005 to 0.005% and

Rem: 0.001 to 0.02%

10. (currently amended) A high-strength hot-rolled steel sheet excellent in shape fixability according to claim 4 ~~or 5~~, wherein the steel sheet is plated.

11. (currently amended) A high-strength hot-rolled steel sheet excellent in shape fixability according to claim 7 ~~or 8~~, wherein the steel sheet is plated.

12. (currently amended) A method of producing a high-strength hot-rolled steel sheet excellent in shape fixability comprising the following steps,

hot-rolling a cast slab having a composition according to claim 4 ~~or 5~~ as cast or cooled once, then reheated to a temperature range of 1000-1300°C, with a total reduction ratio of 25% or more at Ar_3 to (Ar_3+150)°C, temperature at finishing hot-rolling start, TFS, and temperature at finishing hot-rolling end, TFE, simultaneously satisfies following Equations (1) to (4), and

cooling hot-rolled steel sheet, then

coiling at below critical temperature T_0 determined by the chemical composition of the steel sheet shown in the following Equation (5) and a temperature of 400 to 700°C,

$$TFE \geq Ar_3 \tag{1}$$

$$TFE \geq 800°C \tag{1'}$$

$$TFS \leq 1100°C \tag{2}$$

$$20°C \leq TFS - TFE \leq 120°C \tag{4}$$

$$T_0 = -650.4 \times \{C\%/(1.82 \times C\% - 0.001)\} + B \tag{5}$$

where B is found from the composition of the steel expressed by weight %

$$B = -50.6 \times Mneq + 894.3$$

$$Mneq = Mn\% + 0.24 \times Ni\% + 0.13 \times Si\% + 0.38 \times Mo\% + 0.55 \times Cr\%$$

$$+ 0.16 \times Cu\% - 0.50 \times Al\% - 0.45 \times Co\% + 0.90 \times V\%$$

$$Ar_3 = 901 - 325 \times C\% + 33 \times Si\% + 287 \times P\% + 40 \times Al\%$$

$$- 92 \times (Mn\% + Mo\% + Cu\%)$$

$$- 46 \times (Cr\% + Ni\%)$$

13. (original) A method of producing a high-strength hot-rolled steel sheet excellent in shape fixability according to claim 12, characterized by further controlling a friction coefficient to not more than 0.2 in at least one pass in the hot-rolling in a temperature range of Ar_3 to $(Ar_3 + 150)$°C.

14. (original) A method of producing a high-strength hot-rolled steel sheet excellent in shape fixability characterized by applying skin pass rolling of 0.1 to 5% to hot-rolled steel sheet produced by the method of producing a high-strength hot-rolled steel sheet excellent in shape fixability according to claim 12.

15. (currently amended) A method of producing a high-strength hot-rolled steel sheet excellent in shape fixability comprising the following steps,

hot-rolling a cast slab having a composition according to claim 7 ~~or 8~~ as cast or cooled once, then reheated to a range of 1000 to 1300°C, with a total reduction ratios of 25% or more at Ar_3 to $(Ar_3 + 150)$°C, temperature at finishing hot-rolling start, TFS, and temperature at finishing hot-rolling end, TFE, and calculated residual strain $\Delta\varepsilon$ to simultaneously satisfy following relations (1) to (4), and

cooling hot-rolled steel sheet, then

coiling at below critical temperature T_0 determined by the chemical composition of the steel shown in the following relation (5) and a temperature of not more than 400°C:

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$$\text{TFE} \geq \text{Ar}_3 \, (^{\circ}\text{C}) \tag{1}$$

$$\text{TFS} \leq 1100\,^{\circ}\text{C} \tag{2}$$

$$\Delta\varepsilon \geq (\text{TFS}-\text{TFE})/375 \tag{3}$$

$$20\,^{\circ}\text{C} \leq (\text{TFS}-\text{TFE}) \leq 120\,^{\circ}\text{C} \tag{4}$$

$$T_0 = -650.4 \times \{C\%/(1.82 \times C\% - 0.001)\} + B \tag{5}$$

where, B is found from the composition of the steel expressed by weight%,

$$B = -50.6 \times Mneq + 894.3$$

$$Mneq = Mn\% + 0.24 \times Ni\% + 0.13 \times Si\% + 0.38 \times Mo\% + 0.55 \times Cr\%$$

$$+ 0.16 \times Cu\% - 0.50 \times Al\% - 0.45 \times Co\% + 0.90 \times V\%$$

where,

$$Ar_3 = 901 - 325 \times C\% + 33 \times Si\% + 287 \times P\% + 40 \times Al\% - 92$$

$$\times (Mn\% + Mo\% + Cu\%) - 46 \times (Cr\% + Ni\%)$$

$\Delta\varepsilon$ is found from the equivalent strain εi ($\underline{i}$ is 1 to n) given at each stand of the $\underline{n}$ stages of finishing rolling for the rolling, time ti (sec) ($\underline{i}$=1 to $\underline{n}$-1) between stands, time tn (sec) from the final stand to the start of cooling, rolling temperature $Ti(K)$ ($\underline{i}$=1 to $\underline{n}$) at each stand, and a constant R=1.987.

$$\varepsilon = \Delta\varepsilon 1 + \Delta\varepsilon 2 + \cdots + \Delta\varepsilon n$$

$$\text{where, } \Delta\varepsilon i = \varepsilon i \times \exp\{-(ti^*/\tau n)^{2/3}\}$$

$$\tau n = 8.46 \times 10^{-9} \times \exp\{43800/R/Ti\}$$

$$ti^* = \tau n \times (ti/\tau i + t(i+1)/\tau(i+1) + \cdots + tn/\tau n\}$$

16. (original) A method of producing a high-strength hot-rolled steel sheet excellent in shape fixability according to claim 15, characterized by further controlling a friction coefficient to not more than 0.2 in at least one pass in the hot-rolling in a temperature range of Ar_3 to $(Ar_3+150)\,^{\circ}\text{C}$.

17. (original) A method of producing a high-strength hot-rolled steel sheet excellent in shape fixability characterized by applying skin pass rolling of 0.1 to 5% to hot-rolled steel sheet produced by the method of producing a high-strength hot-

rolled steel sheet excellent in shape fixability according to claim 15.